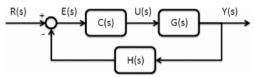
7. Generic Compensators **Electronic Control Systems**



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Problem of Root Locus Design

- Root locus design can locate poles only on the root locus. The method cannot change the root locus and locate poles at desired locations if those desired locations are not on the existing root locus.
- Generic compensators C(s) are used in such situations in order to change the existing root locus



- · There are three generic compensators as
 - Phase lag compensator
 - Phase lead compensator
 - Notch filter

gain is

Phase Lead Compensator

Transfer Function

$$C_{lead}(s) = \frac{s+z}{s+p}; p > z$$

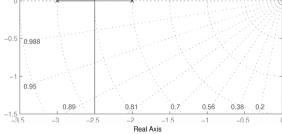
 Phase contribution $\theta_z - \theta_p > 0$

Example

Open loop transfer function of a system is $G(s) = \frac{1}{(s+2)(s+3)}$ Design a control system for the following specifications

- 1.4% overshoot
- 2.1% setting time of 1s

Phase Lead Design s+2)(s+3 Answer The root locus of the feedback control 0 80 0.8 0.38 system with a single feedback 0.5 0.988 $1 + K \frac{1}{(s+2)(s+3)} = 0$



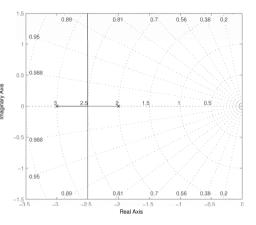
Phase Lead Design

$$\zeta = \sqrt{\frac{(ln0.04)^2}{\pi^2 + (ln0.04)^2}} = 0.72$$
 $\omega_n = \frac{4.6}{1.0 \times 0.72} = 6.39$

Desired poles for required specifications

$$\gamma_1, \gamma_2 = \varsigma \omega_n \pm j \omega_n \sqrt{1 - \varsigma^2}$$
$$= -4.6 \pm j 4.43$$

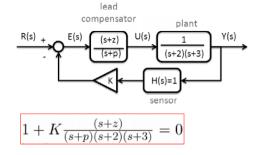
- Poles are outside the root locus
- Gain tuning is not able
 to locate poles



j1

Lead Compensator Design

- Root locus has to be bent to the left. Introduce a lead Compensator
- Characteristic Equation
 with the lead is



• And, at $\gamma_1, \gamma_2 = -4.6 \pm j4.43$ phase condition

$$\angle \frac{(s+z)}{(s+p)(s+2)(s+3)} = \pm 180^{\circ}$$

Lead Compensator Design

$$(180^{0} - 82.3^{0}) - \theta_{p}$$

$$(180^{0} - 70.1^{0}) - (180^{0} - 59.6^{0}) = 180^{0}(2k+1)$$

$$97.7^{0} - \theta_{p} - 109.9^{0} - 120.4^{0} = 180^{0}(2k+1)$$

$$-\theta_{p} - 132.6^{0} = 180^{0}(2k+1)$$

$$-\theta_{p} - 132.6^{0} = -180^{0}; k = 0$$

$$\theta_{p} = 47.4^{0}$$

$$\tan^{-1}\left(\frac{4.43}{p-4.6}\right) = 47.4^{0}$$

$$\frac{4.43}{p-4.6} = 1.09$$

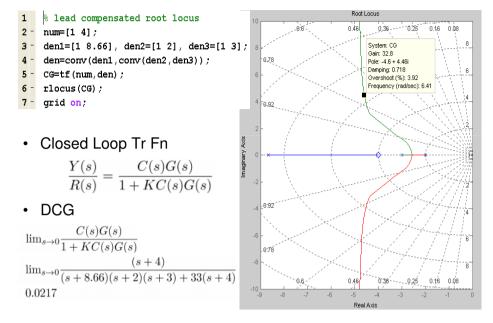
$$\frac{4.43 - 1.09 \times 4.6}{1.09} = p$$

8.66 = p

Lead Compensator Design

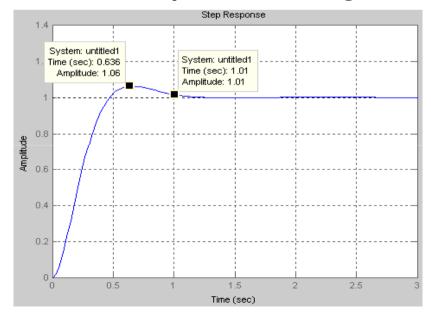
$$-\theta_p - 132.6^0 = 180^0(2k+1)$$
$$-\theta_p - 132.6^0 = -180^0; k = 0$$
$$\theta_p = 47.4^0$$
$$\tan^{-1}\left(\frac{4.43}{p-4.6}\right) = 47.4^0$$
$$\frac{4.43}{p-4.6} = 1.09$$
$$\frac{4.43 - 1.09 \times 4.6}{1.09} = p$$
$$8.66 = p$$

Lead Compensator Design



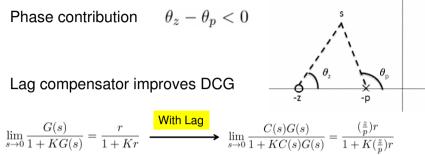
Lead Compensated System lead compensator plant Y(s) (s+4) s+8.66 (s+2)(s+3) H(s)=1 sensor 1 % Step response of lead compensated % system adjusted for DCG=1 2 3 dur=3; K=33; 4 5 num = [1 4];den1=[1 8.66], den2=[1 2], den3=[1 3]; 6 7 den=conv(den1,conv(den2,den3)); 8 G=tf(num,den); 9 sys=feedback(G,K); 10 11 $K = \frac{1}{0.217} = 45.99$ step(45.99*sys,dur); 12 -13 grid on;

Lead Compensator Design



Lag Compensator Design

- Lag transfer function $C_{lead}(s) = \frac{s+z}{s+p}; p < z$
- Phase contribution $\theta_z \theta_p < 0$
- · Lag compensator improves DCG



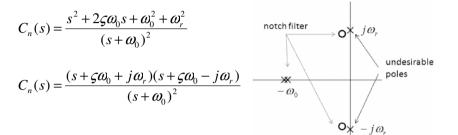
 $z \gg p \qquad \frac{\left(\frac{z}{p}\right)r}{K\left(\frac{z}{z}\right)r} = \frac{1}{K}$

 $r = \lim_{s \to 0} G(s)$

• Lag Compensator is rarely used as it reduces the phase margin in the feedback loop

Notch Filter Design

- · Some plants show sustained oscillations even with a properly designed controller.
- NF can reduce the oscillatory response by way of polezero cancelation method- introducing two complex zeros very close to the oscillatory (pure imaginary) poles.



Notch Filter Design

Example

· Lead compensated feedback plant (previous work) is

$$\frac{Y(s)}{R(s)} = \frac{C(s)G(s)}{1 + KC(s)G(s)} = \frac{46s + 184}{s^3 + 13.66s^2 + 82.3s + 184}$$

Let's introduce a pair of oscillatory poles

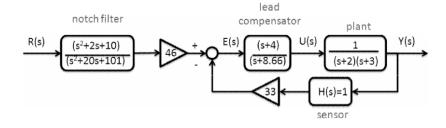
$$\frac{Y(s)}{R(s)} = \frac{46s + 184}{(s^3 + 13.66s^2 + 82.3s + 184)(s^2 + 100)}$$

• NF poles and zeros $s = -1 \pm j10$, and two poles as s = -10

• NF Tr Fn
$$C_{ns} = \frac{(s + (1 - j10))(s + (1 + j10))}{(s + 10)(s + 10)} = \frac{s^2 + 2s + 101}{s^2 + 20s + 100}$$

Notch Filter Design

· Notch filter can be inserted as a cascaded block with the existing feedback control system



Notch Filter Design

	2	-	dur=3; % simulation duration
	3	-	K=33; % feedback gain
	4	-	g=46; % gain for DCG=1
	5	-	wr=10; % freq. of sustained oscillation
	6		
	7		% Lead compensator
	8	-	numL=[1 4]; denL=[1 8.66];
	9	-	Cs=tf(numL,denL);
1	LO		
1	L1		% Plant
1	L2	-	numG=[1]; denG1=[1 2]; denG2=[1 3];
1	L3	-	denG=conv(denG1,denG2);
1	L4	-	Gs=tf(numG,denG);
1	L 5		
1	L6		% feedback control system
1	L7	-	0L=Cs*Gs;
1	L8	-	CL=feedback(OL,K);
1	L9		

Notch Filter Design

20		% Unmodelled sustained oscillation
21	-	$Ps=tf([1],[1 \ 0 \ wr^2]);$
22		
23		% System with oscillation
24	-	sys1=g*CL*Ps;
25	-	<pre>subplot(2,2,1); rlocus(sys1,0); axis([-11 1 -11 11]); grid on;</pre>
26	-	<pre>subplot(2,2,2); step(sys1,dur); grid on;</pre>
27		
28		% Notch filter
29	-	numN1=[1 1+j*wr];numN2=[1 1-j*wr]; numN=conv(numN1,numN2);
30	-	denN=[1 2*wr wr^2];
31	-	N=tf(numN,denN)
32		
33		% System with notch filter
34	-	sys2=N*sys1;
35	-	<pre>subplot(2,2,3); rlocus(sys2,0); axis([-11 1 -11 11]); grid on;</pre>
36	-	<pre>subplot(2,2,4); step(sys2,dur); grid on;</pre>

